Radiation Shielding Materials: Half-value layer determination for separate and simultaneous photon and neutron emissions by a $^{252}$Cf source

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ABSTRACT

Background: The present study aimed to determine half-value layers (HVL) of different materials with neutron, photon, and simultaneous neutron and photon emissions by a $^{252}$Cf source. MCNPX code was used for the simulation of the applicator tube (AT) $^{252}$Cf source and the attenuation materials.

Materials and methods: The $^{252}$Cf source, a source collimator, a detector, a detector collimator, and HVL material were defined in the present study. HVL was determined for lead, concrete, water, polyethylene, and polyethylene mixtures with various concentrations of boric acid for separate neutron, separate photon, and simultaneous emissions of neutron and photon by the $^{252}$Cf source.

Results: HVL values were tabulated for the aforementioned materials for separate neutron, separate photon, and for simultaneous neutron and photon emissions by the $^{252}$Cf source. Among the evaluated materials, polyethylene was the most adequate material for neutron shielding. Conclusion: The obtained HVL results for different materials could be used for shielding design around a $^{252}$Cf source. According to the comparison of lead with concrete, lead was a suitable material for shielding against the photons emission. On the other hand, concrete with a lower HVL value seemed to be superior for neutron shielding. The combination of several HVL layers of polyethylene and lead could result in proper shielding against neutron and photon. In simultaneous neutron and photon emissions, the emitted neutrons from the source generate secondary photons. The issue led to increase HVL, and could be considered in the protection and shielding against the source.

Keywords: HVL, attenuation material, neutron emission, photon emission, $^{252}$Cf source.

INTRODUCTION

As a radioactive material, californium-252 ($^{252}$Cf) is used in a number of industrial applications and the boron neutron capture therapy (BNCT) and for brachytherapy$^{(1-4)}$. Due to the aforementioned applications of $^{252}$Cf, it is important to protect against high energy neutrons and photons that are emitted by this radionuclide and introduction of new shielding materials.

Various studies have been conducted on shielding effects of different materials for protection against neutrons from $^{252}$Cf source$^{(1, 5)}$. Few researchers have paid attention particularly to half-value layer (HVL) values for few shielding materials, but the secondary neutron contribution was neglected$^{(1, 6)}$. HVL is defined as the thickness of material reducing the beam intensity to the half of the original value$^{(7)}$. 
In the aforementioned previous studies, only the HVL against photons and neutrons of $^{252}$Cf were determined for few materials. The past studies had not determined HVL for simultaneous neutrons and photons emissions of $^{252}$Cf source. The evaluation of the past case is important because primary neutrons can generate secondary photons; and primary photons can generate secondary neutrons that affect the thickness of HVL. The present study aimed to obtain HVL for neutron-only, photon-only, simultaneous neutrons and photons emissions and the best material for radiation protection against $^{252}$Cf source.

**MATERIALS AND METHODS**

In the present study, an applicator tube (AT) $^{252}$Cf source (Oak Ridge National Laboratory (ORNL), Oak Ridge, USA) model was simulated using MCNPX Monte Carlo code (version 2.6.0). It is noteworthy that the simulation of this source was validated in a research by the authors; and a validated program was used in the present study (9). In this research a source, a source collimator, a detector, a detector collimator, and HVL materials were defined. Afterwards, HVLs were determined for lead, concrete, water, polyethylene, and polyethylene mixtures with various concentrations of boric acid for three emission modes using the $^{252}$Cf source.

To this end, different thicknesses of the materials were defined in front of this source; and a scoring cell (detector) was placed beyond the attenuating layer; and fluency of particles was obtained before and after the presence of the attenuating layer using F4 tally. To prevent the leakage and scattered rays from reaching the detector, collimators were considered around the source and detector. The input Monte Carlo programs were run for sufficient numbers of particles, so that the fluency calculation uncertainty would be in an acceptable level for all cases. Finally, HVL of different materials were obtained and compared to select appropriate absorbing materials for three emission modes separately.

**Geometry of $^{252}$Cf source**

The ORNL-made AT $^{252}$Cf type consists of an active core, a primary capsule and a secondary capsule. The active core component is a cylinder of Pd: $\text{Cf}_2\text{O}_3$ ceramic metal (10). More details of this source model can be found in previous studies (10, 11). The specifications of $^{252}$Cf including half-life, yield, energy, and dose rate can be considered in a study by Kang et al (11). Fig. 1 shows the geometric arrangement of this source.

**Validation of $^{252}$Cf source simulation**

The present study used the $^{252}$Cf source simulation program that was validated in a previous study by Khosroabadi et al. (9) and here -in a summary of validation of the source simulation is presented. MCNPX (version 2.6.0) simulation code (12) was used to simulate the AT $^{252}$Cf source. Dosimetric parameters of the source were determined according to the presented formalism in the updated American Association of Physicists in Medicine (AAPM) task group No. 43 report (13). The obtained data was compared with the published results of other studies on this source model (14-16). Finally, the source simulation was validated based on this comparison; and the dosimetric results were consistent with other studies.

**HVL determination for neutron emission mode**

Maxwellian fission distribution was used for neutron emission by the $^{252}$Cf source in order to determine HVL. Based on this distribution, the spectrum of emitted neutrons by $^{252}$Cf has an average energy of 2.1 MeV, and the most probable energy of 0.7 MeV (14). Figure 1 shows the HVL determination set-up. For the neutron emission, collimator layers were made of polyethylene, cadmium, polyethylene, lead, lead, cadmium and paraffin for part numbers of 1-7 respectively (figure 1). Collimator materials were selected to absorb scattered particles and prevent them from being counted by the detector (5, 17).

Table 1 presents the compositions and mass densities of these materials as well as HVL materials and they were calculated by the authors according to the table of isotopic masses.
and natural abundances (5, 10, 18). This information is necessary and can be repeated by other researchers. The source collimator tube (layer no. 1) has a length of 130 cm. The thicknesses of layers 2-7 were 0.2 cm, 35 cm, 12 cm, 5 cm, 0.1 cm and 5 cm, respectively. The gas detector was defined as a cylinder with 0.5 cm radius and 1.2 cm height. The detector contained air in the simulations.

For determination of HVL for each material, the particle fluence (primary fluence) was first scored in the detector without the presence of any HVL material on the beam’s path. The thickness of each material was then changed with 1 mm intervals, and the thickness at which the particle fluence had the half of the primary fluence, was calculated. The second digit of HVL value was calculated by interpolation. The neutron spectrum of $^{252}$Cf radionuclide was defined in the source’s active core. The neutrons were transported and F4 tally was scored. No energy cut-off was defined for neutrons. Each input program was run for $10^8$ particles, and the maximum type A uncertainty was 2.77%. It should be noted that the output of MCNP is per source particle, not per number of transported particles. The HVL of neutron was determined for water, lead, concrete, polyethylene, and polyethylene mixture at various concentrations (15%, 25% and 35% weights) of boric acid.

**HVL determination for photon emission mode**

The same method of neutron emission mode was used for the HVL determination for the separate photon cases with differences under which all materials of collimators were made of lead. The photon spectrum of $^{252}$Cf radionuclide was defined in the source’s active core (19). The photons and electrons (due to the production of secondary photons) were transported, and F4 tally was scored for photons in the detector cell. The energy cut-off was 10 keV for the separate photon cases. Each input program was run for $2 \times 10^8$ particles, and the maximum type A uncertainty was 3.22%. The HVL was determined for lead and concrete.

**HVL determination for simultaneous neutron and photon emission mode**

The same method of neutron emission mode was used for the HVL determination for the simultaneous neutron and photon emission mode with differences under which all materials of the collimators layers were made of lead. The neutron and photon spectra of the $^{252}$Cf radionuclide were defined in the active core. Neutrons, photons, and electrons were transported. F4 tally was scored. The energy cut-off of zero, 10 keV and 10 keV were considered for neutrons, photons and electrons, respectively. Two input programs were run for $4 \times 10^8$ and $2 \times 10^8$ particles for neutron and photon, respectively. In the first program of the simultaneous neutron and photon emission, the fluence was scored only for neutron. The fluence was scored only for photons in the second program. The maximum type A uncertainties were 3.77% and 3.65%, respectively, in the HVL determination for neutrons and photons. The HVL was determined for both lead and concrete for neutrons and photons scoring, separately.

![Figure 1.](image-url) The geometric arrangement of the $^{252}$Cf source, source collimator and detector collimator. The figure is not into a real scale.
RESULTS

Table 2 presents HVL values for the $^{252}$Cf source for various materials and four emission modes. As it is presented in table 2 and figure 2, comparisons of HVL values for various materials and four emission modes, the minimum HVL of neutrons and photons emission modes belong to polyethylene and lead, respectively. For simultaneous neutron and photon emission modes, the minimum HVL values belong to concrete and lead when neutron and photon were scored, respectively. The maximum HVL value belongs to concrete (HVL=5.03 cm) for simultaneous neutron and photon emissions mode when photon was scored.
DISCUSSION AND CONCLUSION

For Neutron emission mode, (table 2 and figure 2), the maximum HVL value belongs to lead while polyethylene is the most adequate material for neutron emission mode among the evaluated materials. Due to the addition of boric acid, the inclusion of boric acid simultaneously reduces the percentage of polyethylene in the material, and increases HVL value against neutrons. Since boron captures thermal neutrons, this effect may be due to the fact that fast neutrons have greater contribution to the neutron emission by $^{252}$Cf. In this regard, evaluation of effect of adding other capture agents such as $^{157}$Gd to polyethylene on HVL may be attractive.

Water is also similar to polyethylene. The advantage of water is its availability and low cost. In emergency situations for neutron protection, a $^{252}$Cf source can be put in a water container.

For Photon emission mode, based on the obtained results in the present study, the minimum HVL value belongs to lead (HVL=0.77 cm) for photon emission mode, according to

**Table 2.** HVL values for various materials for neutrons, photons, and spontaneous neutron and photon emissions by $^{252}$Cf source in the present study.

<table>
<thead>
<tr>
<th>Type of source particle</th>
<th>Type of particle for HVL calculation</th>
<th>Material</th>
<th>HVL (cm)-Present study</th>
<th>HVL (cm)-Zarezadeh [5]</th>
<th>Difference (%)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Separate neutron</td>
<td>Neutron</td>
<td>Water</td>
<td>2.16</td>
<td></td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td>Lead</td>
<td>3.35</td>
<td></td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td>Concrete</td>
<td>3.03</td>
<td></td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td>Polyethylene</td>
<td>1.85</td>
<td>1.8</td>
<td>2.0</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Polyethylene and 15% weight boric acid</td>
<td>1.90</td>
<td>1.2</td>
<td>37.0</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Polyethylene and 25% weight boric acid</td>
<td>1.95</td>
<td>1.4</td>
<td>28.0</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Polyethylene and 35% weight boric acid</td>
<td>2.03</td>
<td>1.4</td>
<td>31.0</td>
</tr>
<tr>
<td>Separate photon</td>
<td>Photon</td>
<td>Lead</td>
<td>0.77</td>
<td></td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td>Concrete</td>
<td>4.80</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Simultaneous neutron and photon</td>
<td>Neutron</td>
<td>Lead</td>
<td>3.45</td>
<td></td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td>Concrete</td>
<td>2.80</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Simultaneous neutron and photon</td>
<td>Photon</td>
<td>Lead</td>
<td>0.82</td>
<td></td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td>Concrete</td>
<td>5.03</td>
<td></td>
<td></td>
</tr>
</tbody>
</table>
evaluation of lead and concrete. In comparison, for neutron emission mode in the lead and concrete evaluation, concrete with a lower HVL value seems to be superior for neutron shielding. Therefore, since the density of lead (11.35 g/cm$^3$) is higher than concrete (2.3 g/cm$^3$), lead occupied less space than concrete in terms of volume. In summary, lead is a good absorber of photons of $^{252}$Cf and this is accounted as its advantage if the cost consideration is not taken into account. It can be concluded that a combination of several HVL layers of polyethylene and lead can result in proper shielding against neutron and photon for a $^{252}$Cf source.

For simultaneous neutron and photon emission mode, as it is presented in table 2 and figure 2, the minimum HVL value belongs to concrete and lead when neutron and photon were scored, respectively. In this mode, the HVL of photons were higher than HVL of photons in separate photon emission modes for both lead and concrete. However, it should be noted that the differences are minor. This effect suggests that neutrons, which are emitted from the source, generate secondary photons; and this issue could be considered in protection and shielding against this source. A similar effect is not seen for HVL of neutrons for lead and concrete materials.

Based on the data presented in table 2 and figure 2, a comparison between HVL values can be performed. In summary, the minimum and maximum HVL for separate neutron emission mode belong to polyethylene (HVL=1.85 cm) and lead (HVL=3.35 cm), respectively. The minimum and maximum HVL for separate photon emission mode belong to lead (HVL=0.77 cm) and concrete (HVL=4.80 cm), respectively. The HVLs for the simultaneous neutron and photon mode when neutron is scored for concrete and lead are 2.80 cm and 3.45 cm, respectively. The HVLs for the simultaneous neutron and photon mode when photon is scored for lead and concrete are 0.82 cm and 5.03 cm, respectively.

In a study by Zarezadeh (5), HVL was determined for neutron emission of $^{252}$Cf source by experimental measurement of different mixtures of polyethylene and boric acid. In this study, the data related to polyethylene is in good agreement with the HVL data for polyethylene in table 2. In the case of mixture of polyethylene and boric acid, higher HVL values are observed in the present study due to the increased weight percentage of boric acid, while a decreasing HVL was seen in the study by Zarezadeh. Since relatively similar geometries were used in these two studies, these differences could be related to the uncertainties in the Monte Carlo or experimental measurements.

The results of the present study and those reported by Da Silva and Crispim (6) cannot be compared because there are some differences between the methods of the present study and the research by Da Silva and Crispim (6) in terms of the final evaluated quantities, the types of materials, and the type of presentation of the results (table versus curves).

The present study offer basic practical information about the selection of neutron and photon shielding materials for fuel transport casks, nuclear reactor panel design and the use of $^{252}$Cf source in neutron brachytherapy and BNCT (1). According to the conducted studies on the HVL for neutrons and photons of $^{252}$Cf source, such types of materials have not been considered for shielding evaluations. HVL for photons of this source has not been evaluated yet. It can be concluded that different materials can have advantages and disadvantages in terms of HVL thickness, cost, construction, and space occupation.

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Conflicts of interest: Declared none.
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