

# Dosimetric accuracy of the Acuros XB and Anisotropic analytical algorithm near interface of the different density media for the small fields of a 6- MV flattening -filter-free beam

S.W. Kang<sup>1</sup>, J.B. Chung<sup>2\*</sup>, J.W. Lee<sup>3</sup>, M.J. Kim<sup>1</sup>, Y.L. Kim<sup>4</sup>,  
J.S. Kim<sup>2</sup>, K.Y. Eom<sup>2</sup>, I.A. Kim<sup>2</sup>, T.S. Suh<sup>1\*</sup>

<sup>1</sup>Department of Biomedical Engineering and Research Institute of Biomedical Engineering, College of Medicine, The Catholic University of Korea, Korea

<sup>2</sup>Department of Radiation Oncology, Seoul National University Bundang Hospital, Seongnam, Korea

<sup>3</sup>Department of Radiation Oncology, Kunkuk University Medical Center, Korea

<sup>4</sup>Department of Radiologic Technology, Choonhae College of Health Sciences, Ulsan 689-784, Korea

## ABSTRACT

**Background:** This study was conducted to assess the accuracy of dose calculation near the air-phantom interface of a heterogeneous phantom for Acuros XB (AXB) and Anisotropic Analytical Algorithm (AAA) algorithm of a 6-MV flattening-filter-free beam, compared with film measurements.

**Materials and Methods:** A phantom included air gap was specially manufactured for this study. In order to evaluate the dose near air gap-phantom interface, Eclipse treatment planning system equipped both AXB and AAA was used for the dose calculations. Measurements in this region were performed with radiochromic film. The central-axis dose (CAD) and off-axis dose (OAD) between calculations and measurements were analyzed for various field sizes and air gaps. The root-mean-square-error (RMSE) was used to evaluate the difference between the calculated and measured OAD. In order to quantify agreement between the calculated and measured dose distributions, the gamma analysis was performed with the 2%/2 mm and 3%/3 mm criteria. **Results:** For all fields traveling through 1 and 3 cm air gap, the maximum difference in the calculated CAD was -5.3% for AXB and 214.8% for AAA, compared to the measured CAD. For the RMSE between the calculated and measured OAD, the calculated OAD using AXB showed interval in the RMSE (from 4.4 to 12.7) while using AAA indicated broad (from 7.7 to 101.0). In addition, the gamma passing rates showed that AXB was higher agreement than AAA. **Conclusion:** This study demonstrated that AXB was more accurate in heterogeneous media near air-phantom interface than AAA when comparing the measured data.

**Keywords:** Acuros XB, anisotropic analytical algorithm, heterogeneous media, FFF, interface.

## ► Original article

### \*Corresponding authors:

Dr. Jin-Beom Chung,

Dr. Tae. S. Suh,

### E-mail:

jbchung1213@gmail.com

suhsanta@catholic.ac.kr

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## INTRODUCTION

An air gap-tissue interface irradiated by high energy photon has a transition area in which the electron fluence is composed of electrons generated in both media <sup>(1)</sup>. Radiation dose at proximate air cavity-tissue interfaces has been

long a subject of investigation. However, to measure dose at the interface was difficult due to lack of electronic equilibrium <sup>(2)</sup>. These electron disequilibrium cause an inaccurate radiation therapy. Several investigators reported that the under dosing occurs in treatment of head and neck cancer due to the presence of air

cavities<sup>(3-7)</sup>. On the other hand, the under dosing that gives rise to the skin-sparing effect could reduce the dose delivered to the rectal wall during treatment of prostate cancer, as reported by Holmes *et al.*<sup>(1)</sup>.

Unfortunately, conventional dose calculation algorithms such as Pencil Beam Convolution Algorithm (PBC) and Anisotropic Analytical Algorithm (AAA) implemented in the current widely used treatment planning systems (TPS) cannot predict the accurate dose in the heterogeneous region including the different density materials as well as the interface between air cavities and tissues.

In recent, the Acuros XB (AXB) which called a new photon dose calculation algorithm was implemented in Eclipse TPS (Varian Medical System, Palo Alto, CA). The AXB algorithm solves deterministically the coupled system of linear Boltzmann transport equations (LBTEs) that describes the macroscopic behavior of radiation particles as they travel through and interact with matter. Some researchers stated that the AXB provides more fast and accurate in heterogeneous media as well as homogenous media than the AAA using comparisons with measurement and Monte Carlo (MC) calculations<sup>(7-10)</sup>. Fogliata *et al.* concluded that AXB provides a valid and accurate alternative to MC simulations for small and large fields. In the previous study, we demonstrated that the dose calculation results using AXB on a phantom containing an air cavity was within 5% compared to the film measurement data for small fields travelling through air cavity with a 6-MV flattened (FF) beam<sup>(11)</sup>.

In this study, we compared the accuracy of AXB and AAA against film measurements near air gap-phantom interface on heterogeneous phantom for small fields of a 6-MV flattening-filter-free (FFF) beam. To the best of our knowledge, only one paper was published the results of comparison between the calculated and measured percentage depth dose (PDD) curve but the study included not the analysis about the off-axis dose (OAD)<sup>(12)</sup>. Therefore, we included the evaluation about the off-axis dose (OAD) as well as the central-axis dose (CAD). Furthermore, we analyzed the

agreement between the calculated and measured dose distribution with both gamma criteria.

The aim of this study was to assess the dosimetric accuracy of AXB dose calculation near air-phantom interface of a heterogeneous phantom using a comparison with AAA and film measurements for small fields of a 6-MV FFF beam.

## MATERIALS AND METHODS

### *Phantom with an air gap*

The acryl ( $\rho=1.14 \text{ g/cm}^3$ ) phantom included an air gap was used to evaluate the accuracy of dose calculation for both AAA and AXB dose calculation algorithms. The overall dimensions of the heterogeneous phantom were  $20 \times 20 \times 13.5 \text{ cm}^3$ . The phantom was composed to two types which has 1 and 3 cm air gap, respectively, as shown in figure 1. The phantom was scanned using a Philips Big-bore computed tomography (CT) scanner (Philips, Healthcare Andover, MA) with a slice thickness of 3 mm. The digital imaging and communications in medicine (DICOM) CT datasets of the phantom were then transferred to the Eclipse TPS (version 11.0.34, Varian Medical Systems, Palo Alto, CA).

### *Calculation of the central-axis dose and off-axis dose*

By the phantom setup shown in figure 1, the central-axis dose (CAD) and off-axis dose (OAD) was calculated in interface (position A) and rebuild-up regions (position B and C) beyond air gap of the phantom for four field sizes from  $2 \times 2 \text{ cm}^2$  to  $5 \times 5 \text{ cm}^2$ . The position A indicates the air-phantom interface. The position B and C indicate the regions of 3 and 5 mm depth beyond air gap within the heterogeneous phantom.

All dose computations were performed with both AAA and AXB dose calculation algorithms equipped in Eclipse TPS for a 6-MV FFF beam of TrueBeam linear accelerator (Varian Medical Systems, Palo Alto, CA, USA). A dose of 400 cGy was delivered at maximum dose depth (1.5 cm) by 100 cm source-to-surface distance (SSD). The

calculation grid size of 0.1 cm was used to improve the dose calculation accuracy.

### Measurement of the central axis dose and off axis dose

Measurement of the CAD and OAD was performed on the heterogeneous phantom with radiochromic film (EBT3, the same batch, Lot #: 3171401). The CAD, OAD, and dose distributions were measured in position A, B and C under the same condition of calculations in

TPS.

For the film dosimetry, a net-optical density (netOD) curve for a 6-MV FFF beam was obtained with a 10×10 cm<sup>2</sup> field size. Doses ranging from 0 to 900 cGy were used to acquire the calibration curve of the film. After irradiated 24 hours, the films were scanned with a flatbed scanner (Epson Expression 11000 XL, Epson America Inc., Long Beach, CA) for analyzing the measured CAD, OAD, and dose distributions.

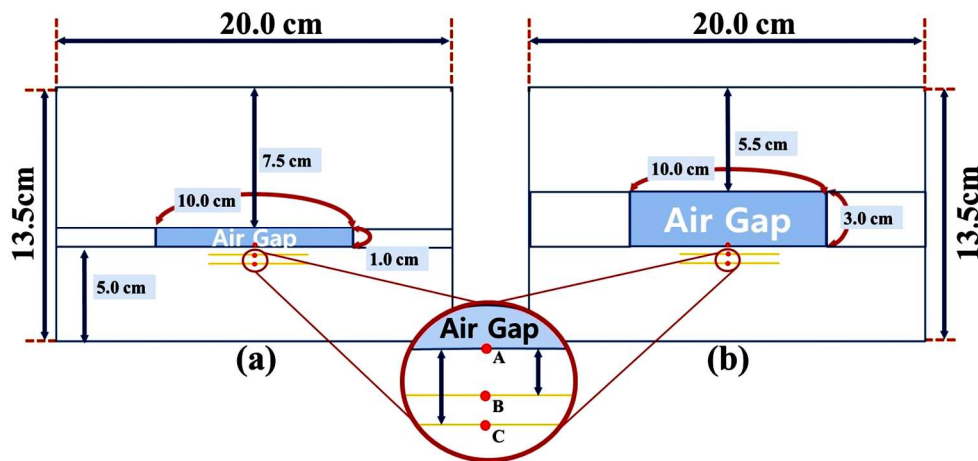


Figure 1. The inhomogeneous phantom with two air gap thickness; (a) 1 and (b) 3 cm gap thickness.

### Analysis between the calculated and measured data

For analysis of the calculated CAD and OAD, the calculated results which were acquired in TPS were resized into the same resolution of the measured data by the interpolation method. With matching the calculated CAD, the percentage difference (%Diff) in the calculated CAD against the measured CAD was evaluated across four field sizes and three positions. The % Diff was expressed as the following equation (1):

$$\%Diff_{AXB \text{ or } AAA} = \frac{(CAD_{AXB \text{ or } AAA} - CAD_{meas})}{CAD_{meas}} \times 100 \quad (1)$$

Also, the difference between the calculated and measured OAD was evaluated with the function of the root-mean-square-error (RMSE). The RMSE was defined as the following Equation (2):

$$RMSE_{AXB \text{ or } AAA} = \sqrt{\frac{\sum_{i=1}^N ((OAD_{AXB \text{ or } AAA} - OAD_{meas})^2)}{N}} \quad (2)$$

where, N is the total point number for the OAD.  $OAD_{AXB \text{ or } AAA}$  represents the calculated OAD by AXB or AAA algorithm and  $OAD_{meas}$  is the measured OAD by film.

In order to quantify the agreement between the calculated and measured dose distributions, a 3-D gamma analysis was performed as described by Moran *et al.* (13). The gamma analysis applied the modified gamma index ( $\Gamma_m$ , Equation 3), which adds the generalized gradient ( $G_e$ ) to the conventional gamma equation. The  $G_e$  (Equation 4), which combines all local gradients at the evaluated point ( $r_e$ ) with the nearest surrounding point ( $r_j$ ), is calculated from the dose difference ( $\Delta d_{re-rj}$ ) and grid spacing ( $\Delta d_{re-rj}$ ) between the evaluated point ( $r_e$ ) and the nearest point ( $r_j$ ) in the evaluated matrix (14).

$$\Gamma_m(r_r, r_e) = \sqrt{\left(\frac{r(r_r, r_e)}{\Delta d_M}\right)^2 + \left(\frac{|\Delta D(r_r, r_e) - G_e d_{gc}|}{\Delta D_M}\right)^2},$$

$$r(r_r, r_e) = |r_r - r_e|, \Delta D(r_r, r_e) = D_r(r_r) - D_e(r_e), \quad (3)$$

$$G_e = \sqrt{\sum_j \left(\frac{\Delta d_{r_e - r_j}}{\Delta x_{r_e - r_j}}\right)^2} \quad (4)$$

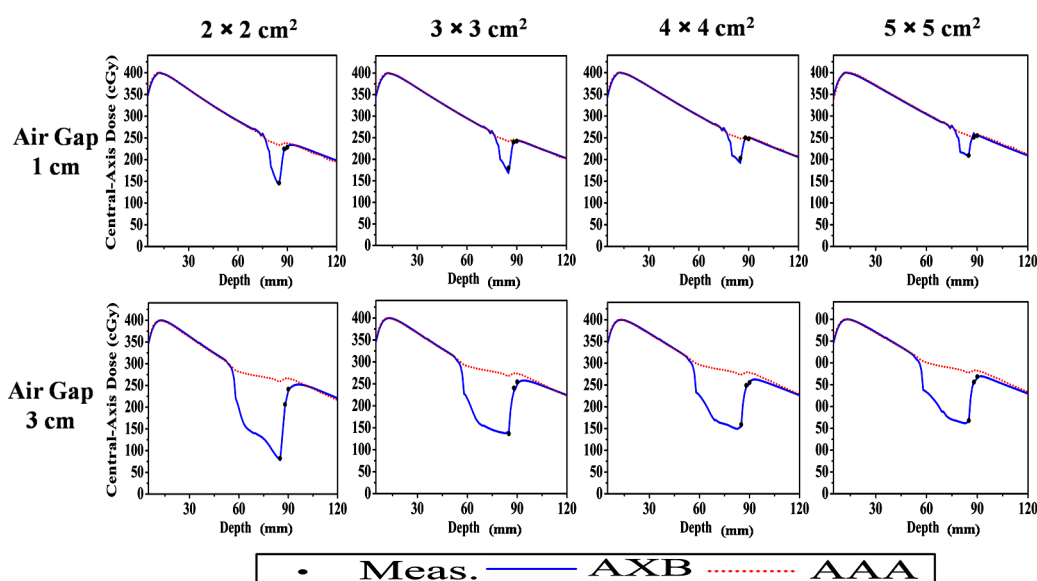
The 3D gamma agreement was evaluated with the criteria of distance to agreement ( $\Delta d_M$ ) of 2 mm and dose difference ( $\Delta D_M$ ) of 2% (2%/2 mm) and 3%/3 mm.

## RESULTS

### The calculated and measured central axis dose

Figure 2 shows a comparison with the

measured and calculated CAD at position A, B, and C for the field sizes ranging from  $2 \times 2$  to  $5 \times 5$  cm<sup>2</sup> on the phantom included 1 and 3 cm air gap. Table 1 presents the percentage difference between the measured and calculated CAD for four fields traversing through both air gaps. When comparing the measured CAD at the position A for all fields, the maximum percentage difference in the calculated CAD using AXB for 1 and 3 cm air gap was -6.6% for the  $3 \times 3$  cm<sup>2</sup> field size and -5.3% for the  $2 \times 2$  cm<sup>2</sup> field size, respectively. Whereas, the percentage difference in the calculated CAD using AAA ranged from 21.6% to 59.5% for 1 cm air gap and from 65.5% to 214.8% for 3 cm air gap, depending on various field sizes.



**Figure 2.** The calculated and measured central-axis dose near air-phantom interface beyond air gap of (a) 1 and (b) 3 cm within heterogeneous phantom for four field sizes.

In the position B and C, the average percentage difference in the calculated CAD using AXB for all fields was 1.02% and -1.16% for 1 and 3 cm air gap. The corresponding value in the calculated CAD using AAA was 2.1% and 12.1%, respectively.

The calculated and measured off-axis dose. Figure 3 and 4 show the comparison results between the measured and calculated OAD at three positions relative to air gap and field size for both algorithms. Table 2 summarizes the

RMSE value between the calculated and measured OAD at three positions depending on field size and air gap.

Compared to the measured OAD, the RMSE values in the calculated OAD using AXB were within 12.6 cGy for 1 cm air gap, whereas corresponding values in the calculated CAD using AAA were more than 53.8 cGy. Overall, the RMSE value in the calculated OAD using AXB at the position A was higher than that of B and C position for the same field size, except at the  $2 \times$



2 cm<sup>2</sup> field size (RMSE value at A position: 4.4 cGy, at B and C position: 6.5 and 7.4 cGy, respectively). The RMSE values in 3 cm air gap were higher than those in 1 cm air gap for both algorithms. The maximum RMSE value in the calculated OAD using AXB and AAA compared to the measured OAD was 14.5 and 101.0 cGy. It was observed at the position A of the 3 × 3 cm<sup>2</sup> field size for AXB and the 5 × 5 cm<sup>2</sup> field size for

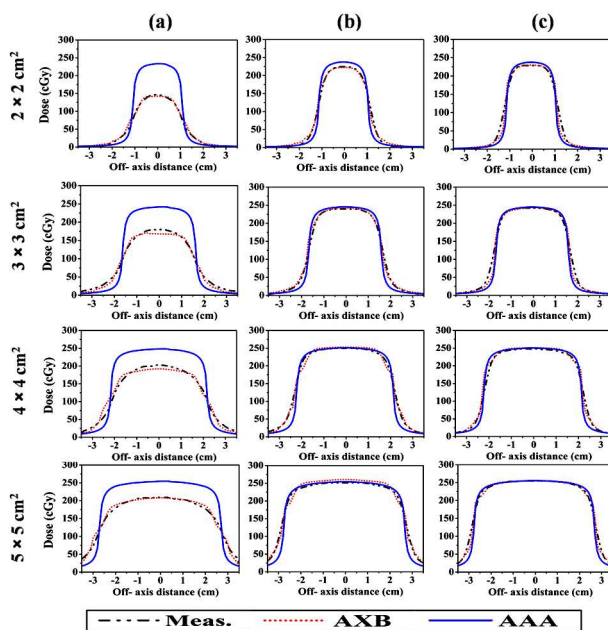
AAA.

As shown in figure 3 and 4, the relatively high dose difference between the calculated and measured OAD was obtained in the out-of-field than in-field. The difference for both algorithms was increased with increasing field size and air gap compared to the measured OAD. Furthermore, the difference was reduced with increasing measurement depth (position C).

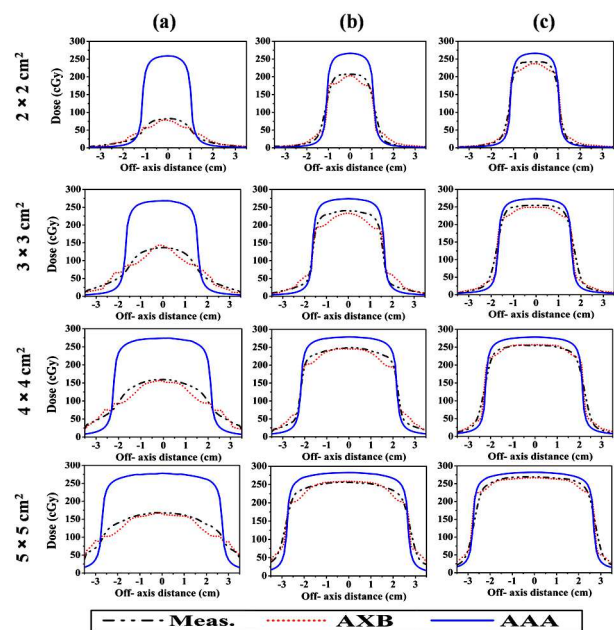
**Figure 2.** The calculated and measured central-axis dose near air-phantom interface beyond air gap of (a) 1 and (b) 3 cm within heterogeneous phantom for four field sizes.

|                       |          | Dose (cGy)   |       |       |              |       |       | %Diff        |      |              |       |
|-----------------------|----------|--------------|-------|-------|--------------|-------|-------|--------------|------|--------------|-------|
|                       |          | 1 cm air gap |       |       | 3 cm air gap |       |       | 1 cm air gap |      | 3 cm air gap |       |
|                       | Position | Meas.        | AXB   | AAA   | meas         | AXB   | AAA   | AXB          | AAA  | AXB          | AAA   |
| 2 × 2 cm <sup>2</sup> | A*       | 146.4        | 142.5 | 233.6 | 82.4         | 78.0  | 259.3 | -2.7         | 59.5 | -5.3         | 214.8 |
|                       | B*       | 224.6        | 222.7 | 237.8 | 206.9        | 203.3 | 266.2 | -0.8         | 5.9  | -1.7         | 28.7  |
|                       | C*       | 228.6        | 229.9 | 237.6 | 242.0        | 237.3 | 266.1 | 0.6          | 3.9  | -2.0         | 10.0  |
| 3 × 3 cm <sup>2</sup> | A        | 179.7        | 167.9 | 242.0 | 136.6        | 142.2 | 268.4 | -6.6         | 34.6 | 4.1          | 96.6  |
|                       | B        | 239.8        | 242.7 | 245.6 | 240.1        | 233.1 | 274.1 | 1.2          | 2.4  | -2.9         | 14.2  |
|                       | C        | 242.0        | 243.2 | 244.9 | 254.5        | 249.1 | 273.4 | 0.5          | 1.2  | -2.1         | 7.4   |
| 4 × 4 cm <sup>2</sup> | A        | 202.8        | 192.2 | 248.3 | 159.3        | 154.6 | 274.1 | -5.2         | 22.5 | -2.9         | 72.1  |
|                       | B        | 250.0        | 252.9 | 251.2 | 249.1        | 245.7 | 279.1 | 1.2          | 0.5  | -1.4         | 12.1  |
|                       | C        | 247.6        | 251.0 | 250.5 | 255.1        | 256.9 | 278.5 | 1.4          | 1.2  | 0.7          | 9.2   |
| 5 × 5 cm <sup>2</sup> | A        | 209.4        | 207.8 | 254.6 | 167.9        | 165.6 | 277.9 | -0.8         | 21.6 | -1.4         | 65.5  |
|                       | B        | 251.3        | 260.6 | 254.4 | 256.0        | 258.6 | 282.7 | 3.7          | 1.2  | 1.0          | 10.4  |
|                       | C        | 255.0        | 256.3 | 255.7 | 269.1        | 266.7 | 282.2 | 0.5          | 0.3  | -0.9         | 4.9   |

\*A: air-phantom distal interface, B and C : 3 and 5 mm depths below air cavity.



**Figure 3.** Comparison between the measured and calculated off-axis dose at each position for all fields traversing through a 1 cm air gap.



**Figure 4.** Comparison between the measured and calculated off-axis dose at each position for all fields traversing through a 3 cm air gap.

| Field size                |    | 1 cm air gap |      |  | 3 cm air gap |       |
|---------------------------|----|--------------|------|--|--------------|-------|
|                           |    | AXB          | AAA  |  | AXB          | AAA   |
| $2 \times 2 \text{ cm}^2$ | A* | 4.4          | 51.2 |  | 6.6          | 93.7  |
|                           | B* | 6.5          | 16.5 |  | 12.3         | 33.7  |
|                           | C* | 7.4          | 9.1  |  | 10.9         | 16.7  |
| $3 \times 3 \text{ cm}^2$ | A  | 10.1         | 53.8 |  | 14.5         | 91.9  |
|                           | B  | 7.2          | 15.7 |  | 11.5         | 28.6  |
|                           | C  | 6.4          | 8.5  |  | 10.9         | 16.5  |
| $4 \times 4 \text{ cm}^2$ | A  | 12.6         | 52.5 |  | 12.7         | 96.3  |
|                           | B  | 7.4          | 17.9 |  | 12.4         | 30.6  |
|                           | C  | 8.4          | 8.4  |  | 10.0         | 21.4  |
| $5 \times 5 \text{ cm}^2$ | A  | 9.3          | 51.8 |  | 11.8         | 101.0 |
|                           | B  | 9.3          | 18.2 |  | 11.4         | 31.5  |
|                           | C  | 7.7          | 7.7  |  | 10.9         | 16.2  |

\*A: air-phantom distal interface, B and C : 3 and 5 mm depths below air cavity.

**Table 3.** Gamma passing rate between the calculated and measured dose distributions evaluated with 2%/2 mm and 3%/3 mm criteria at all selected positions for all fields traversing through 1 and 3 cm air gap.

| Field size                |    | 1cm air gap |        |        |        | 3cm air gap |        |        |        |
|---------------------------|----|-------------|--------|--------|--------|-------------|--------|--------|--------|
|                           |    | AXB         |        | AAA    |        | AXB         |        | AAA    |        |
|                           |    | 2%/2mm      | 3%/3mm | 2%/2mm | 3%/3mm | 2%/2mm      | 3%/3mm | 2%/2mm | 3%/3mm |
| $2 \times 2 \text{ cm}^2$ | A* | 75.6        | 99.1   | 4.1    | 12.1   | 62.5        | 90.0   | 2.5    | 13.6   |
|                           | B* | 80.6        | 98.2   | 18.8   | 44.7   | 71.2        | 91.9   | 17.2   | 31.5   |
|                           | C* | 90.0        | 99.5   | 66.9   | 83.7   | 86.7        | 93.9   | 23.8   | 48.1   |
| $3 \times 3 \text{ cm}^2$ | A  | 78.0        | 97.5   | 4.1    | 6.1    | 61.4        | 94.2   | 2.7    | 11.8   |
|                           | B  | 84.2        | 98.6   | 70.6   | 81.2   | 76.0        | 97.7   | 11.9   | 30.1   |
|                           | C  | 94.1        | 98.8   | 81.2   | 87.8   | 94.8        | 99.5   | 18.8   | 38.4   |
| $4 \times 4 \text{ cm}^2$ | A  | 77.2        | 99.5   | 2.5    | 5.6    | 76.9        | 86.4   | 5.1    | 10.3   |
|                           | B  | 85.1        | 99.7   | 80.0   | 86.7   | 82.9        | 97.6   | 9.9    | 22.0   |
|                           | C  | 94.8        | 99.6   | 84.7   | 91.5   | 96.7        | 99.6   | 11.5   | 23.7   |
| $5 \times 5 \text{ cm}^2$ | A  | 80.4        | 99.3   | 3.8    | 6.0    | 80.1        | 93.2   | 0.2    | 3.0    |
|                           | B  | 87.0        | 100.0  | 87.8   | 98.5   | 87.2        | 98.5   | 7.2    | 17.5   |
|                           | C  | 99.0        | 100.0  | 93.6   | 97.7   | 98.3        | 99.2   | 9.5    | 34.9   |

\*A: air-phantom interface, B and C : 3 and 5 mm depth below air gap within heterogeneous phantom.

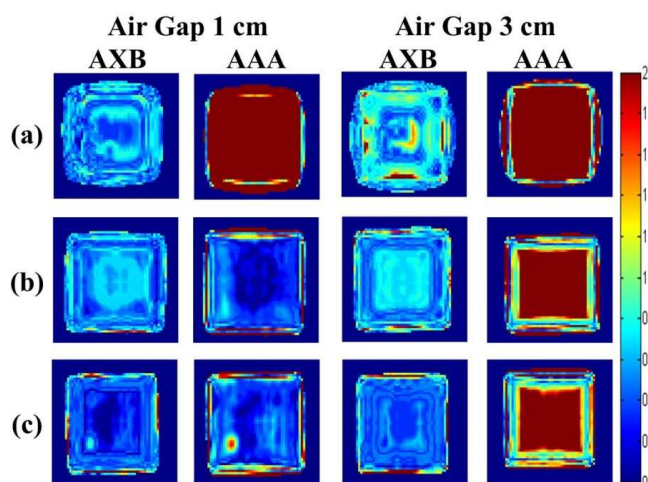
### Gamma evaluation

Figure 5 and table 3 show agreement between the calculated and measured dose distribution. The calculated dose distribution using AXB was better agreement than that of AAA. As shown in Table 3, the passing rate for all fields and air gaps indicated higher agreement in the calculated dose distribution using AXB than AAA.

For all fields traversing through a 1 cm air gap, the passing rates for AXB ranged from 75.6% to 99.0% for a criterion of 2%/2 mm, whereas the corresponding values for AAA

ranged from 4.1% to 93.6%. The passing rate for AXB and AAA was increased as increasing the measured depth as shown in table 3. In the position A, the maximum passing rate between the calculated and measured dose distribution was 80.4% for AXB and 4.1% for AAA. In the position C, the passing rate was 99.0% for AXB and 93.6% for AAA.

For both algorithms, the passing rates were decreased with increasing air gap. In a 3 cm air gap, the maximum passing rates of the calculated dose distribution using AXB and AAA was 98.3% and 23.8% for the 2%/2 mm criteria.



**Figure 5.** Gamma distribution evaluated with the 3%/3mm criteria at position A, B, and C for the  $4 \times 4$  cm<sup>2</sup> field traversing through 1 and 3 cm air gap. The color bar indicates the gamma-index levels.

The gamma passing rate at the position C was significantly decreased in the calculated dose distribution using AAA than AXB.

In all positions (A, B, and C), the passing rates of the calculated dose distribution using AXB for the 3%/3 mm criteria were more than 90.0% for two air gaps and all fields tested, excepted 86.4% at A position for the  $4 \times 4$  cm<sup>2</sup> field. The passing rates of the calculated dose distribution using AXB for the 2%/2 mm criteria were mostly closed than 80%. On the other hand, the passing rates of the calculated dose distribution using AAA for all positions showed a wide range (from 5.6 to 98.5 for a 1 cm air gap and from 3.0 to 48.1 for a 3 cm air gap) depending on the field size, and air gap.

## DISCUSSION

Many studies reported on the accuracy verification of the different dose calculation algorithms to heterogeneous media as well as homogeneous medium<sup>(18-22)</sup>. Some studies demonstrated that the AXB was more accurate with measurement in heterogeneous phantom than AAA<sup>(5, 18, 19)</sup>. Kan *et al.*<sup>(18)</sup> also indicated that the differences of AXB was within 7.5% at the different material interface of the heterogeneous phantom compared to TLD measurement for clinical IMRT, whereas those of the AAA overestimated more than 11.0%. With clinical

aspect, Chung *et al.*<sup>(20)</sup> presented that the AXB was more accurate than the AAA at dose calculation in lung stereotactic ablative radiotherapy (SABR).

We also evaluated the accuracy on the calculated dose of AXB and AAA respect to film measurement. The verification for both algorithms was performed as a function of field size and air gap with a phantom included air gap, specially using a 6-MV FFF beam. To our knowledge, no study has compared the dosimetric accuracy between the different dose calculation algorithms and measurements for FFF beams.

Our results demonstrated that AXB was lower difference than AAA in the calculated CAD and OAD compared to the measured data (table 1). For the position A, B, and C, the calculated CAD using AXB was observed the differences of the narrow (within -6.6% for 1 cm air gap and -5.3 for 3 cm air gap) interval with the measured CAD as a function of field size, while AAA has the relatively (up to 214.8% for 3 cm air gap) broad differences. In results from the previous two studies, the AXB was the difference of the calculated CAD within 7.3% on a phantom included an air gap against the measured CAD.<sup>(18)</sup> Rana *et al.*, also reported that the differences in CAD between AXB calculations and measurements ranged from -3.81% to 0.9% across the several air gap thickness (2, 4, and 6 cm) for three field sizes ( $3 \times 3$ ,  $5 \times 5$ , and  $10 \times 10$

cm<sup>2</sup>) using a 6-MV photon beam. However, there was no the regular trend for the difference between the calculated and measured CAD as changing the field size and air gap. Our results are in line with this finding.

In RMSE used to evaluate the calculated and measured OAD, the maximum value in RMSE relative to the field size and air gap was 12.7 for AXB and 101.0 cGy for AAA, respectively. It presented in the position A which was air-phantom interface adjacent the different densities. The RMSE value of both algorithms was decreased with increasing field size and reducing air gap thickness compared to the measurement. The remarkable difference was observed in the out-of-field of profile for the AAA than the AXB, as shown figures 3 and 4. The discrepancy was explained that AAA did not model the effect of lateral electronic disequilibrium. For inhomogeneity correction in the heterogeneous media, the AAA was considered with two parameters which were independently scaled depth-directed and lateral components. The depth-directed component was scaled by calculating radiologic distance between the surface and the point of interest, whereas the lateral component calculated the path length from the central of the beamlet in the water equivalent environment. The divergent scatter of heterogeneities from the upper levels was incorporated correctly. In contrast, the AXB is able to calculate the interactions of radiation particle within the heterogeneity media by using LBTE. Therefore, the AXB can perform dose calculations with the material assignment for each voxel distinguished by the Hounsfield unit (HU) of the CT image <sup>(23, 24)</sup>.

In this study, gamma evaluation was performed to compare agreement between the calculated and measured dose distributions. This gamma analysis has been widely accepted and provides the means for an efficient analysis. Our study indicated that the AXB calculations were good agreement with the measured results than AAA for both criteria in spite of variations of the field size and air gap (figure 5 and table 3). For three selected positions, the highest passing rate in both algorithms was observed in

position C which had the deepest depth. The lowest passing rate was shown in interface (position A) as in CAD and RMSE. In the previous study reported by Kan *et al.* <sup>(25)</sup>, there was also low gamma passing rates in the air-tissue interface.

In this study, all measurements in our heterogeneous phantom were made with radiochromic EBT3 film. Therefore, the results were obtained at depth which included the film thickness. They were not exactly the doses at air-phantom interface although the differences between calculations and measurements were not large. Moreover, the film dosimetry had a disadvantage which requires the well-controlled calibration procedure. However, it was a well-estimated method for verifying both absolute dose and dose distribution.

## CONCLUSION

With using a phantom including air gaps, the accuracy of dose calculation algorithm of AAA and AXB was evaluated with film measurement for small fields and three positions near air-phantom interface. Our study found that the AXB was more accurate dose calculation algorithm than the AAA compared to the measured dose according to variations of field size and air gap when considering a heterogeneous media, especially included air gap. Therefore, the results of this study suggest that the AXB must be used in heterogeneous media such as human body where include significantly different densities for achieving accurate dose calculation.

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